

Project Godre'graig School Spoil Options				Job no. 50084	
Calcs for Embedded Retaining Wall				Start page no./Revision 1	
Calcs by BG	Calcs date 08/07/2021	Checked by KJ	Checked date	Approved by	Approved date

### EMBEDED PILE WALL ANALYSIS & DESIGN

In accordance with BS EN1997-1:2004 - Code of Practice for Geotechnical design and the UK National Annex

Tedds calculation version 2.0.02

#### Design summary

##### Combination 1

Description	Unit	Provided	Required	Utilisation	Result
Total length required	mm	14000	11069	1.265	PASS
Maximum moment in pile 458.8 kNm/mx2.5m(King Post spacing)=1147KNm					
Maximum shear in pile 395.6 kN/mx2.5m(King Post spacing)=989KN					

##### Combination 2

Description	Unit	Provided	Required	Utilisation	Result
Total length required	mm	14000	12038	1.163	PASS
Maximum moment in pile 431.2 kNm/mx2.5m(King Post spacing)=1078KNm					
Maximum shear in pile 353.6 kN/mx2.5m(King Post spacing)=884KN					

#### Geometry

Length of pile provided	$H_{pile} = 14000$ mm	No. of different types of soil	$N_s = 2$
Retained height	$d_{ret} = 4000$ mm	Unplanned excavation depth	$d_{ex} = 0$ mm
Total retained height	$d_s = 4000$ mm	Angle of retained slope	$\beta = 30.0$ deg
Water depth retained side	$d_w = 8000$ mm	Water depth retaining side	$d_{wp} = 4000$ mm

#### Loading

Variable surcharge  $p_{o,Q} = 5.0$  kN/m<sup>2</sup>

#### Soil characteristic properties table

Soil	$\phi'_k$ (deg)	$\delta_k$ (deg)	$\gamma_m$ (kN/m <sup>3</sup> )	$\gamma_s$ (kN/m <sup>3</sup> )	h (mm)
1	28.0	18.7	10.0	19.0	10000
2	30.0	20.0	15.0	20.0	7000

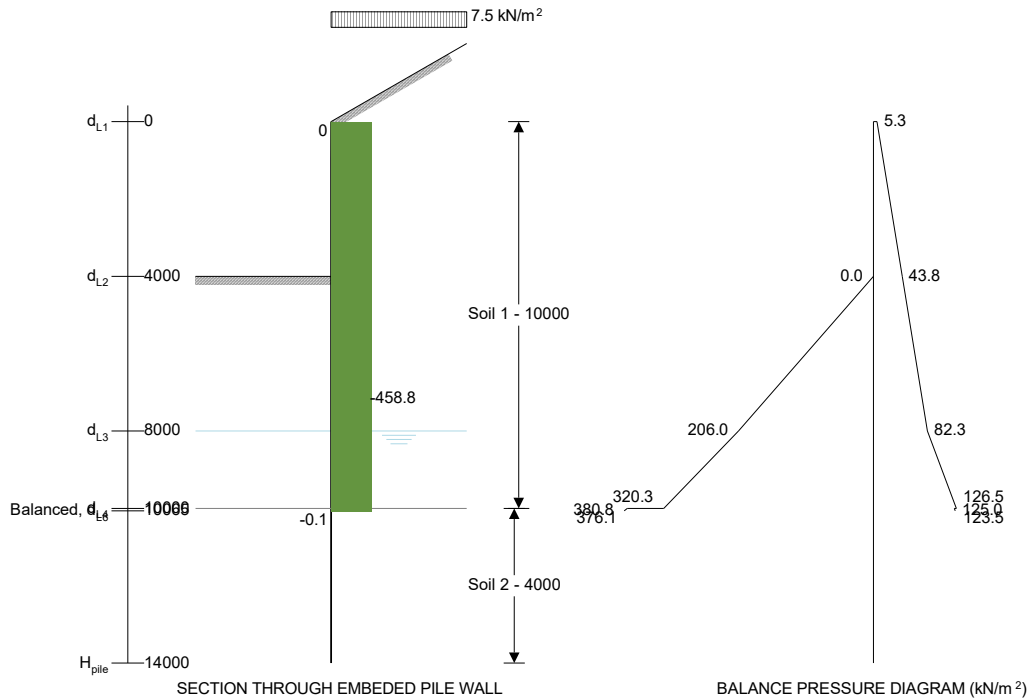
#### Partial factors on actions - Section A.3.1 - Combination 1

Perm. unfavourable action	$\gamma_G = 1.35$	Perm. favourable action	$\gamma_{G,f} = 1.00$
Vari. unfavourable action	$\gamma_Q = 1.50$		
Angle of shearing resistance	$\gamma_\psi = 1.00$	Weight density	$\gamma_\gamma = 1.00$

#### Design properties table - combination 1

Soil	$\phi'_d$	$\delta_d$	$\gamma_{m,d}$	$\gamma_{s,d}$	$K_a$	$K_p$
1	28.0	18.7	10.0	19.0	0.823	5.151
2	30.0	20.0	15.0	20.0	0.798	6.105

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**Overburden on active side**

OB at 0 mm - soil 1	OB' <sub>a11</sub> = 7.5 kN/m <sup>2</sup>	OB at 4000 mm - soil 1	OB' <sub>a21</sub> = 61.5 kN/m <sup>2</sup>
OB at 8000 mm - soil 1	OB' <sub>a31</sub> = 115.5 kN/m <sup>2</sup>	OB at 10000 mm - soil 1	OB' <sub>a41</sub> = 140.3 kN/m <sup>2</sup>
OB at 10000 mm - soil 2	OB' <sub>a42</sub> = 140.3 kN/m <sup>2</sup>	OB at 10065 mm - soil 2	OB' <sub>a51</sub> = 141.2 kN/m <sup>2</sup>

**Overburden on passive side**

OB at 4000 mm - soil 1	OB' <sub>p21</sub> = 0.0 kN/m <sup>2</sup>	OB at 8000 mm - soil 1	OB' <sub>p31</sub> = 40.0 kN/m <sup>2</sup>
OB at 10000 mm - soil 1	OB' <sub>p41</sub> = 58.4 kN/m <sup>2</sup>	OB at 10000 mm - soil 2	OB' <sub>p42</sub> = 58.4 kN/m <sup>2</sup>
OB at 10065 mm - soil 2	OB' <sub>p51</sub> = 59.0 kN/m <sup>2</sup>		

**Pressure on active side**

Active at 0 mm - soil 1	p' <sub>a11</sub> = 5.3 kN/m <sup>2</sup>	Active at 4000 mm - soil 1	p' <sub>a21</sub> = 43.8 kN/m <sup>2</sup>
Active at 8000 mm - soil 1	p' <sub>a31</sub> = 82.3 kN/m <sup>2</sup>	Active at 10000 mm - soil 1	p' <sub>a41</sub> = 126.5 kN/m <sup>2</sup>
Active at 10000 mm - soil 2	p' <sub>a42</sub> = 123.5 kN/m <sup>2</sup>	Active at 10065 mm - soil 2	p' <sub>a51</sub> = 125.0 kN/m <sup>2</sup>

**Pressure on passive side**

Passive at 4000 mm - soil 1	p' <sub>p21</sub> = 0.0 kN/m <sup>2</sup>	Passive at 8000 mm - soil 1	p' <sub>p31</sub> = 206.0 kN/m <sup>2</sup>
Passive at 10000 mm - soil 1	p' <sub>p41</sub> = 320.3 kN/m <sup>2</sup>	Passive at 10000 mm - soil 2	p' <sub>p42</sub> = 376.1 kN/m <sup>2</sup>
Passive at 10065 mm - soil 2	p' <sub>p51</sub> = 380.8 kN/m <sup>2</sup>		

**By iteration the depth at which the active moments equal the passive moments has been determined as 10065 mm as follows:-**

**Active moment about 10065 mm**

Moment level 1	M <sub>a11</sub> = 93.3 kNm/m	Moment level 1	M <sub>a12</sub> = 648.5 kNm/m
Moment level 2	M <sub>a21</sub> = 414.8 kNm/m	Moment level 2	M <sub>a22</sub> = 559.5 kNm/m
Moment level 3	M <sub>a31</sub> = 115.1 kNm/m	Moment level 3	M <sub>a32</sub> = 92.6 kNm/m
Moment level 4	M <sub>a41</sub> = 0.2 kNm/m	Moment level 4	M <sub>a42</sub> = 0.1 kNm/m

**Passive moment about 10065 mm**

Moment level 2	M <sub>p21</sub> = 0.0 kNm/m	Moment level 2	M <sub>p22</sub> = 1400.5 kNm/m
Moment level 3	M <sub>p31</sub> = 288.2 kNm/m	Moment level 3	M <sub>p32</sub> = 234.5 kNm/m

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Moment level 4  $M_{p41} = 0.5 \text{ kNm/m}$       Moment level 4  $M_{p42} = 0.3 \text{ kNm/m}$

**Total moments about 10065 mm**

Total active moment  $\Sigma M_a = 1924.0 \text{ kNm/m}$       Total passive moment  $\Sigma M_p = 1924.0 \text{ kNm/m}$

**Required pile length**

Length reqd to balance mnts  $H = 10065 \text{ mm}$       Depth of equal pressure  $d_{contra} = 5046 \text{ mm}$

Add 20% below this point  $d_{e\_add} = 6023 \text{ mm}$       Minimum required pile length  $H_{total} = 11069 \text{ mm}$

**Pass - Provided length of pile greater than minimum required length of pile**

**Partial factors on actions - Section A.3.1 - Combination 2**

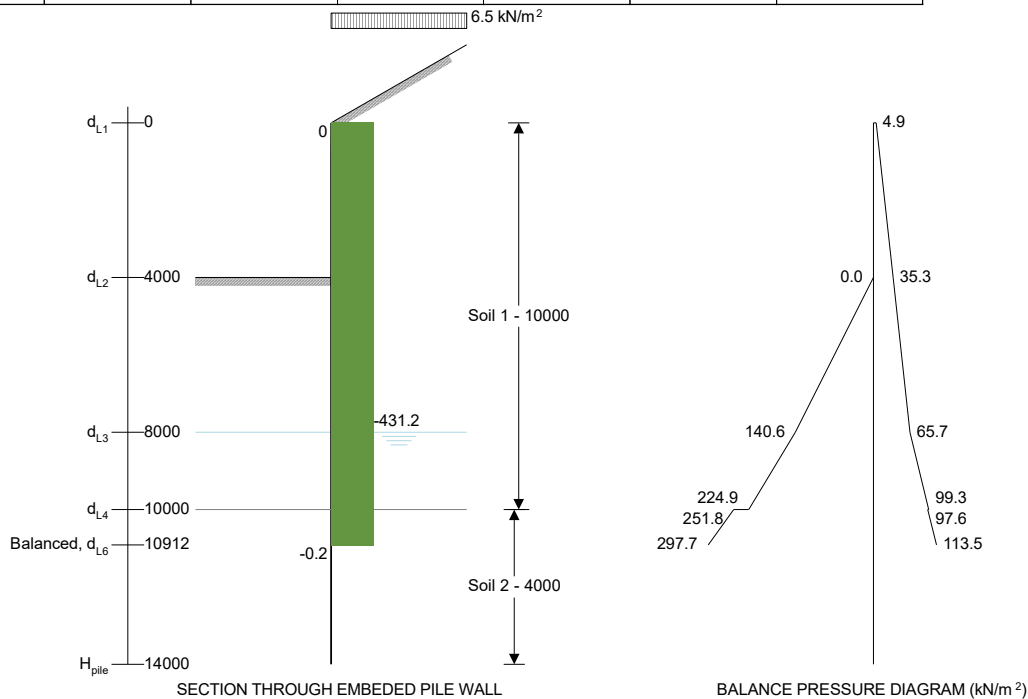
Perm. unfavourable action  $\gamma_G = 1.00$       Perm. favourable action  $\gamma_{G,f} = 1.00$

Vari. unfavourable action  $\gamma_Q = 1.30$

Angle of shearing resistance  $\gamma_\psi = 1.25$       Weight density  $\gamma_\gamma = 1.00$

**Design properties table - combination 2**

Soil	$\phi'_d$	$\delta_d$	$\gamma_{m,d}$	$\gamma_{s,d}$	$K_a$	$K_p$
1	23.0	15.1	10.0	19.0	0.877	3.516
2	24.8	16.2	15.0	20.0	0.858	3.977



**Overburden on active side**

OB at 0 mm - soil 1  $OB'_{a11} = 6.5 \text{ kN/m}^2$       OB at 4000 mm - soil 1  $OB'_{a21} = 46.5 \text{ kN/m}^2$

OB at 8000 mm - soil 1  $OB'_{a31} = 86.5 \text{ kN/m}^2$       OB at 10000 mm - soil 1  $OB'_{a41} = 104.9 \text{ kN/m}^2$

OB at 10000 mm - soil 2  $OB'_{a42} = 104.9 \text{ kN/m}^2$       OB at 10913 mm - soil 2  $OB'_{a51} = 114.2 \text{ kN/m}^2$

**Overburden on passive side**

OB at 4000 mm - soil 1  $OB'_{p21} = 0.0 \text{ kN/m}^2$       OB at 8000 mm - soil 1  $OB'_{p31} = 40.0 \text{ kN/m}^2$

OB at 10000 mm - soil 1  $OB'_{p41} = 58.4 \text{ kN/m}^2$       OB at 10000 mm - soil 2  $OB'_{p42} = 58.4 \text{ kN/m}^2$

OB at 10913 mm - soil 2  $OB'_{p51} = 67.7 \text{ kN/m}^2$

**Pressure on active side**

Active at 0 mm - soil 1  $p'_{a11} = 4.9 \text{ kN/m}^2$       Active at 4000 mm - soil 1  $p'_{a21} = 35.3 \text{ kN/m}^2$

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Active at 8000 mm - soil 1  $p'_{a31} = 65.7 \text{ kN/m}^2$       Active at 10000 mm - soil 1  $p'_{a41} = 99.3 \text{ kN/m}^2$   
Active at 10000 mm - soil 2  $p'_{a42} = 97.6 \text{ kN/m}^2$       Active at 10913 mm - soil 2  $p'_{a51} = 113.5 \text{ kN/m}^2$

**Pressure on passive side**

Passive at 4000 mm - soil 1  $p'_{p21} = 0.0 \text{ kN/m}^2$       Passive at 8000 mm - soil 1  $p'_{p31} = 140.6 \text{ kN/m}^2$   
Passive at 10000 mm - soil 1  $p'_{p41} = 224.9 \text{ kN/m}^2$       Passive at 10000 mm - soil 2  $p'_{p42} = 251.8 \text{ kN/m}^2$   
Passive at 10913 mm - soil 2  $p'_{p51} = 297.7 \text{ kN/m}^2$

**By iteration the depth at which the active moments equal the passive moments has been determined as 10912 mm as follows:-**

**Active moment about 10912 mm**

Moment level 1	$M_{a11} = 94.6 \text{ kNm/m}$	Moment level 1	$M_{a12} = 582.5 \text{ kNm/m}$
Moment level 2	$M_{a21} = 394.1 \text{ kNm/m}$	Moment level 2	$M_{a22} = 558.0 \text{ kNm/m}$
Moment level 3	$M_{a31} = 147.6 \text{ kNm/m}$	Moment level 3	$M_{a32} = 156.8 \text{ kNm/m}$
Moment level 4	$M_{a41} = 27.1 \text{ kNm/m}$	Moment level 4	$M_{a42} = 15.7 \text{ kNm/m}$

**Passive moment about 10912 mm**

Moment level 2	$M_{p21} = 0.0 \text{ kNm/m}$	Moment level 2	$M_{p22} = 1194.3 \text{ kNm/m}$
Moment level 3	$M_{p31} = 315.9 \text{ kNm/m}$	Moment level 3	$M_{p32} = 355.1 \text{ kNm/m}$
Moment level 4	$M_{p41} = 69.9 \text{ kNm/m}$	Moment level 4	$M_{p42} = 41.3 \text{ kNm/m}$

**Total moments about 10912 mm**

Total active moment	$\Sigma M_a = 1976.5 \text{ kNm/m}$	Total passive moment	$\Sigma M_p = 1976.5 \text{ kNm/m}$
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**Required pile length**

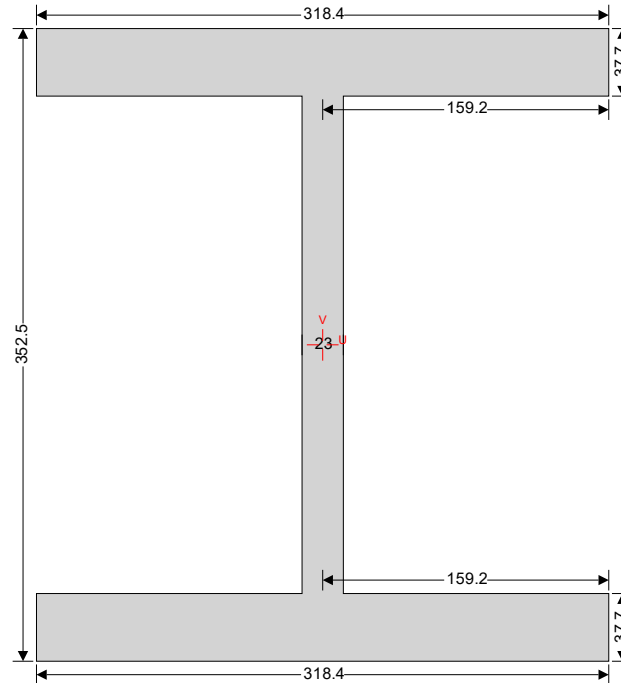
Length reqd to balance mnts	$H = 10912 \text{ mm}$	Depth of equal pressure	$d_{contra} = 5282 \text{ mm}$
Add 20% below this point	$d_{e\_add} = 6757 \text{ mm}$	Minimum required pile length	$H_{total} = 12038 \text{ mm}$

***Pass - Provided length of pile greater than minimum required length of pile***

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Calcs for King Pspot Steel Section Property				Start page no./Revision 5	
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**CALCULATION OF SECTION PROPERTIES-305x305x240UC (Grade S355)**

Tedds calculation version 2.0.07



**Area**

$A = 303.81 \text{ cm}^2$

**2<sup>nd</sup> moment of area**

$I_{uu} = 63.8 \times 10^3 \text{ cm}^4$

$I_{vv} = 20.3 \times 10^3 \text{ cm}^4$

$I_{xx} = 63.8 \times 10^3 \text{ cm}^4$

$I_{yy} = 20.3 \times 10^3 \text{ cm}^4$

**Radius of gyration**

$r_{uu} = 145.0 \text{ mm}$

$r_{vv} = 81.8 \text{ mm}$

$r_{xx} = 14.5 \text{ cm}$

$r_{yy} = 8.2 \text{ cm}$

**Plastic section modulus (only shapes with all rectangles at 90 degs)**

$S_{xx} = 4.22 \times 10^3 \text{ cm}^3$

$S_{yy} = 1.95 \times 10^3 \text{ cm}^3$

**Distance to combined centroid**

$X_e = 0.0 \text{ mm}$

$Y_e = 0.0 \text{ mm}$

Design bending resistance moment - eq 6.13;  $M_{c,Rd} = M_{pl,Rd} = W_{pl,y} \cdot f_y / \gamma_{M0} = 1465.2 \text{ kNm}$

Design shear resistance - cl 6.2.6(2);  $V_{c,Rd} = V_{pl,Rd} = A_v \cdot (f_y / \sqrt{3}) / \gamma_{M0} = 1710 \text{ kN}$

Based on the embedded retaining wall design calculation presented in the previous pages, the maximum bending and shear force as a result of the ULS design value of actions are as follows:

Med:1147kNm <  $M_{pl,Rd} = 1465.2 \text{ kNm}$  Bending Check OK

Ved:989 kN <  $V_{pl,Rd} = 1710 \text{ kN}$  Shear Check OK

Deflection check for the pile section to be undertaken by the pile designer.